ASSIGNMENTS and ANSWERS

dcm 10/24/2018

<table>
<thead>
<tr>
<th>week</th>
<th>notes</th>
<th>assignment</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td></td>
<td>2.21, 2.23, 2.33, 4.15, 4.20</td>
</tr>
<tr>
<td>2</td>
<td></td>
<td>4.2, 4.4, 4.16, 6.6, 7.1, 7.2, 7.6, 7.9, 7.13</td>
</tr>
<tr>
<td>3</td>
<td></td>
<td>(see handout)</td>
</tr>
<tr>
<td>4</td>
<td></td>
<td>9.2, 9.5, 9.6, 9.8, 9.14</td>
</tr>
<tr>
<td>5</td>
<td></td>
<td>(see handout)</td>
</tr>
<tr>
<td>6</td>
<td></td>
<td>midterm #1 (see handout)</td>
</tr>
<tr>
<td>7</td>
<td></td>
<td>(see handout)</td>
</tr>
<tr>
<td>8</td>
<td></td>
<td>(see handout)</td>
</tr>
<tr>
<td>9</td>
<td></td>
<td>12.1, 12.2, 12.3 (optional Jensen-Haise)</td>
</tr>
<tr>
<td>10</td>
<td></td>
<td>10.3, 10.6, 10.7 (optional Richards), 10.12</td>
</tr>
<tr>
<td>11</td>
<td></td>
<td>midterm #2 (see handout)</td>
</tr>
<tr>
<td>12</td>
<td></td>
<td>(see handout)</td>
</tr>
<tr>
<td>13</td>
<td></td>
<td>(see handout)</td>
</tr>
<tr>
<td>14</td>
<td></td>
<td>(see handout)</td>
</tr>
</tbody>
</table>

Answers (not in “Back of Book”)
These partial answers will help determine whether you are on track. Some have been rounded.

Week 1
2.21 (a) 380 kg, (c) 1600 kg, (e) 1900 kg
2.23 3.55 g/cm³
2.33 short essay
4.15a hint, assume given pressure values are suction. When P = -0.10 bar, θ = 34%.
4.15b hint, “plant available water” is “field capacity” minus “permanent wilting point,” where all three are measured in units of moisture content θ. Field capacity is the moisture content after gravity has removed all the water it can. Permanent wilting point is the moisture content below which crops fail; below this moisture content crops cannot be revived by adding water. Assume the permanent wilting point is half the field capacity (https://www.decagon.com/en/support/how-do-i-determine-field-capacity/ 9/7/2016).
4.20 hint, assume “equilibrium” means total head constant throughout column

Week 2
4.16 hint, the CGS system uses cm, g, and s (in contrast to the MKS system’s m, kg, and s)
7.1 correction, problem statement should be for mobility $k/\eta = 4.15 \times 10^{-7}$ m² Pa⁻¹ s⁻¹.
7.13 hint, think about continuity
**Week 3**

1. *hint*, recall definition of derivative: \( \frac{dy}{dx} = \lim_{\Delta x \to 0} \frac{y\mid_{x+\Delta x} - y\mid_{x}}{\Delta x} \)
2. answers will vary
3. answers will vary
4. Brooks and Corey’s (1966) parameter \( n = 1.9 \) optimized by least squares
5. van Genuchten’s (1980) parameter \( m = 1.1 \) optimized by least squares
6. based on the root mean squared error (RMSE), both methods are equivalent here

**Week 4**

9.14 *hint*, assume \( \theta_{\text{surface}} = \theta_{\text{air}} \). (a) \( E_{\text{cum}} = 2.2 \text{ cm} \). (b) required solar flux 53-55 MJ/(m²d).

**Week 5**

1-2 answers given in problem statement

**Week 6**

1. After running HYDRUS-1D, you should get the following for \( h(\theta) \) and \( K(\theta) \):

   **Hydraulic Properties: Head vs. Theta**

   ![Graph of Hydraulic Properties: Head vs. Theta]

   **Hydraulic Properties: K vs. Theta**

   ![Graph of Hydraulic Properties: K vs. Theta]

   Your plots of \( h(z) \), \( \theta(z) \), and \( K(z) \) should resemble Figures 13.3, 13.4, and 13.5.
2 (optional Fall 2018)

$\theta(z)$ should match the following, where $T_0 = 0 \text{ hr}$, $T_1 = 8 \text{ hr}$, $T_2 = 48 \text{ hr}$, and $T_3 = 240 \text{ hr}$:

**Profile Information: Water Content**

Week 7

11.4 *hint*, using corrected equations in errata list, your plot should resemble Figure 11.8

Week 8

1 essay answers will vary

3 $S = 120 \text{ m}$

4 (a) $S = 190 \text{ m}$ for ditches, and $170 \text{ m}$ for perforated pipes

(b) *hint*, allowable infiltration $R_{max}$ depends on your selected $h_o$.

Week 9

12.1 *hints*

- download evaporation data from [http://www.ucdenver.edu/dmays/5335](http://www.ucdenver.edu/dmays/5335)
- for multiple regression, use Microsoft Excel’s `LINEST` function
  - because `LINEST` cannot handle missing values, you will need to filter the data
  - equations (12.32)-(12.35) are erroneous

12.2 at $z = 3,000 \text{ m}$, $P \approx 144 \text{ mm}$, and $T \approx 6.9 \, ^\circ\text{C}$

12.3 *hints*

- assume Table 12.7 is for northern latitudes (shift by 6 months for southern latitudes)
- for pan evaporation, assume a 100 m fetch of upstream alfalfa

Week 10

10.3 *note*, average linear velocity should be $v$ not $q$, so $v = q/\theta = (Q/A)/\theta = 0.317 \text{ cm/hr}$.

*note*, equation (10.24) should be $D = vL/(4\pi S^2) = 0.13 \text{ cm}^2/\text{hr}$ not $0.63 \text{ cm}^2/\text{hr}$.

10.6 *note*, equation (10.51) has solubility $S \, [\text{mg/L}]$ and organic carbon partitioning coefficient $K_{oc} \, [\text{mL/g}] = [\text{L/kg}]$. Accordingly, the partitioning coefficient $K$ is also $[\text{mL/g}] = [\text{L/kg}]$.

* Finally, re-defining $S$, we have sorbed concentration $S \, [\mu g/g] = [\text{mg/kg}]$.

10.12 1.9 years
**Week 11**

1. *hint*, in Excel, calculate \( A = \frac{R_x - vt}{2\sqrt{D_R}t} \), then \( \text{erf}(A) \), then \( \text{erfc}(A) \). Repeat for \( B = \frac{R_x + vt}{2\sqrt{D_R}t} \).

2. (Fall 2018, disregard “TCE” results below)

**Part D: Normalized Concentration Profile**

*Diagram showing normalized concentration profile with axes labeled.*

**Part F: Normalized Breakthrough Curve**

*Diagram showing normalized breakthrough curve with axes labeled.*

**Week 12**

1. Results given below, where \( T_0 = 0 \) d, \( T_1 = t_L/2 = 85 \) d, \( T_2 = t_L = 170 \) d, and \( T_3 = 365 \) d.

**Week 13**

1. answers will vary
2. (a) answers will vary
   (b) *hint*, visit [http://www.ucdenver.edu/dmays/3414](http://www.ucdenver.edu/dmays/3414)
3. answers will vary

**Week 14**

1. *hint*, sand is 60% by mass and 1% by surface area
2. *hint*, assuming \( d = 1 \) μm and \( \rho = 2.5 \) g/cm³, \( s = 801.6 \) m²/g for primary particles
3. *hint*, for chemical condition F, illite is dispersed, and the other clays are flocculated
4. *hint*, sketch how electrostatic repulsive potential \( \Psi_R \) changes with ionic strength
5. answers will vary